



Technical Note

# Local-Scale Horizontal CO<sub>2</sub> Flux Estimation Incorporating Differential Absorption Lidar and Coherent Doppler Wind Lidar

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**Abstract:** A micro-pulse lidar system incorporating differential absorption lidar (DIAL) and coherent Doppler wind lidar (CDWL) is proposed and demonstrated. Due to the high signal-to-noise ratio (SNR) of the superconducting nanowire single-photon detector (SNSPD), the DIAL channel achieves high sensitivity in CO<sub>2</sub> measurement. Meanwhile, the CDWL channel is used to obtain the horizontal wind field. In the process of the optimization and calibration of the DIAL receiver, specifically, mode scrambling and temperature control of the connecting fiber between the telescope and the SNSPD enhance the stability and robustness of the system. Horizontal scanning of the CO<sub>2</sub> concentration and the wind field is carried out in a 6 km range over a scanning span of 60° with a radial resolution of 150 m and 15 s. The results show that the hybrid lidar system captures the spatial distribution of CO<sub>2</sub> concentration and the wind field simultaneously. The horizontal net CO<sub>2</sub> flux in a radius of 6 km is estimated by integrating the CO<sub>2</sub> concentration and the wind transport vector, indicating different characteristics of horizontal net CO<sub>2</sub> fluxes in an industrial area, a university campus, and a park. During most of the experiment, CO<sub>2</sub> flux remained positive in the industrial area, but balances fell to nearly zero on the campus and in the park. The horizontal net fluxes averaged over 24 h in the three areas are  $3.5 \times 10^5$  ppm·m<sup>2</sup>·s<sup>-1</sup>,  $0.7 \times 10^5$  ppm·m<sup>2</sup>·s<sup>-1</sup>, and  $0.1 \times 10^5$  ppm·m<sup>2</sup>·s<sup>-1</sup>.

**Keywords:** differential absorption lidar; coherent Doppler wind lidar; CO<sub>2</sub> concentration; CO<sub>2</sub> flux; SNSPD



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## 1. Introduction

Quantifying the sources and sinks of carbon dioxide (CO<sub>2</sub>) in the atmosphere is of great significance for controlling climate warming and studying atmospheric composition [1–6]. The current emission and absorption of CO<sub>2</sub> in the atmosphere are still subject to large uncertainties [7–9]. Flux observations can be used to analyze CO<sub>2</sub> transport processes.

Spaceborne instruments can infer large-scale global carbon fluxes by imaging surface radiation [10,11]. Eddy covariance technique can measure the vertical flux of carbon dioxide directly [12,13]. By approaching average CO<sub>2</sub> and water vapor mixing ratios in the atmospheric boundary layer as quasi-equilibrium, net CO<sub>2</sub> surface exchange can be estimated [14]. The Lagrangian budgeting approach was used to quantify the uptake of CO<sub>2</sub> [15]. Flux profiles over larger areas usually require networks of tall towers, balloons, or airborne-based flight to obtain average fluxes with spatial resolutions ranging from tens to hundreds of square kilometers [16–19]. However, for areas with less than 1 km<sup>2</sup> or

non-uniform (mixed) coverage, the measurement is quite difficult, and footprint models are required to improve the representativeness [20].

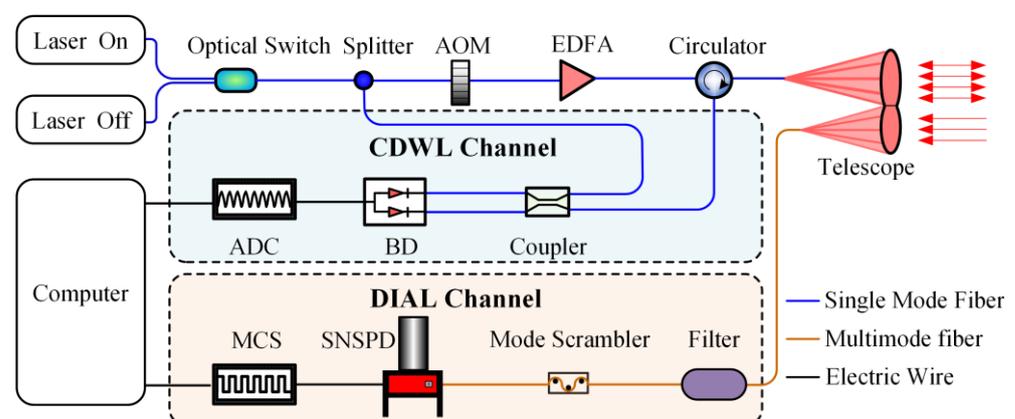
Due to high spatial and temporal resolution, the lidar technique has significant advantages in the remote sensing of aerosol particles [21], gas concentrations [22–27], and wind fields [28]. There have been many reports on gas detection based on differential absorption lidar (DIAL) [29–31] and Raman lidar [32,33]. Thus, the flux in any local area within the measurement range can be observed. Studies on gas flux based on lidar technique have been reported. The vertical flux of water vapor was measured using coherent DIAL and CDWL [34,35]. The vertical aerosol flux was measured using Doppler and Raman lidars [36]. Meanwhile, the vertical flux of CO<sub>2</sub> induced by turbulence was estimated based on coherent DIAL, using the eddy covariance technique [37]. However, compared with direct detection, the signal-to-noise ratio (SNR) of coherent lidar is greatly affected by speckle noise, which limits the accuracy of the measured gas concentration. The vertical flux of CO<sub>2</sub> above a crater was estimated using path-integrated CO<sub>2</sub> concentration and the vertical plume transport speed derived from video analysis [38]. By scanning the cross-section of a CO<sub>2</sub> plume from a stack, incorporating wind in the orthogonal direction, CO<sub>2</sub> emission was measured [39].

Although there have been studies of CO<sub>2</sub> flux measurement, the dynamic monitoring of CO<sub>2</sub> horizontal transport is rarely reported. A combination of multiple techniques or instruments is required to achieve the above goals. In this paper, a hybrid lidar incorporating DIAL and coherent Doppler wind lidar (CDWL) is developed to estimate the horizontal CO<sub>2</sub> flux. The instruments and principles are introduced in Section 2. The optimization and calibration of the receiver are described in Section 3. The experiments and results are demonstrated in Section 4. A new method is proposed to estimate the local horizontal flux as shown in Section 4. Finally, a conclusion is drawn in Section 5.

## 2. Instruments and Principles

### 2.1. Instruments

As shown in Figure 1, a compact and hybrid lidar system incorporating a DIAL channel and a CDWL channel has been developed. The DIAL channel is based on molecular spectral differential absorption technology for CO<sub>2</sub> gas detection. The CDWL channel is based on heterodyne detection for wind-field measurement. The two subsystems share the same laser transmitter, optical collimator, and control system but adopt different optical receivers. The detailed parameters of the hybrid lidar are listed in Table 1.



**Figure 1.** A diagram of the hybrid lidar system: AOM, acoustic–optical modulator; EDFA, erbium-doped fiber amplifier; ADC, analog to digital converter; BD, balance detector; SNSPD, superconducting nanowire single-photon detector; MCS, multi-channel scaler.

**Table 1.** Key parameters of the hybrid lidar.

Parameter	Value
On wavelength	1572.335 nm
Off wavelength	1572.454 nm
Pulse energy	80 $\mu$ J
Pulse average power	0.8 W
On/off pulse repetition frequency	5 kHz
On/off laser frequency uncertainty	0.5 MHz
Diameter of collimator	80 mm
Diameter of telescope	70 mm
Spatial resolution	150 m
Radial temporal resolution	15 s
Maximum range	6 km
Azimuth scanning range	0–360°
Zenith scanning range	0–90°
SDE of SNSPD @ 1572 nm	31.5%
Responsibility of BD	1.0 A/W
Sample rate of ADC	500 MS/s

In the transmitting system, the so-called on-wavelength laser and the off-wavelength laser are continuous-wave seed lasers, which alternately emit continuous light with a frequency of 10 kHz under the control of a fast optical switch (OS). After the splitter, one portion of the light is used as a probe laser and another small part is used as a local oscillator laser for heterodyne detection. The probe signal is chopped and frequency-shifted 80 MHz by an acoustic-optical modulator (AOM), ensuring the identical pulse shape for the laser at two wavelengths. After the AOM, the pulsed laser is amplified by an erbium-doped fiber amplifier (Rayshinning, SW-PFL-2  $\times$  1-S/A). After passing through a circulator, the probe laser is transmitted into the atmosphere via a collimator. The atmospheric backscatter is collected by two telescopes.

In the CDWL channel, the backscatter coupled by one telescope (collimator) is redirected to a circulator and then mixed with the local oscillator laser and measured on a balanced detector (BD). The analog signal is converted to digital signal by an analog-to-digital converter (ADC) and then processed by a computer.

In the DIAL channel, the backscatter received from another bi-axis telescope is coupled into a multimode fiber (MMF). After an online optical filter, the signal is modulated by a fiber mode scrambler and then detected by a large-active-area superconducting nanowire single-photon detector (SNSPD) for CO<sub>2</sub> gas detection. The nine-channel analog signal output from the SNSPD is amplified and read out as a digital signal by nine homemade electrical modules. A multi-channel scaler (MCS) records the digital signal, which is then processed by the same computer.

## 2.2. Advantages of the Hybrid Lidar

By sharing a transmitting system, the measured signals in both channels are from the same backscattering volume, and the wind profile and CO<sub>2</sub> concentration are measured synchronously. The probe pulse of two wavelengths differs only in the absorption of the cross-section of the gas under test, avoiding most impacts caused by the atmospheric turbulence effect. Meanwhile, the hybrid lidar, incorporating single-photon DIAL and CDWL, inherits the advantages of both techniques.

CO<sub>2</sub> detection requires high sensitivity. For intensity detection, single-photon detection performed with SNSPD provides higher SNR than that of the coherent technique [30,40]. Meanwhile, an MMF-coupled SNSPD possesses a large active area [41], avoiding the jitter of coupling efficiency from the telescope with a common single-mode fiber. If the coherent technique is adopted, the single-mode detection will be affected by the turbulence, resulting in a jitter from coupling the efficiency of the telescope.

Two approaches of wind measurement by lidar are available: direct detection and coherent detection [28]. For direct detection, an expensive frequency discriminator is required, and the spectrum of Doppler-shifted backscatter is assumed to be an ideal Gaussian shape [28]. A large number of detections show that the spectra exhibit different shapes under the functions of turbulence, wind shear, and rainfall [42]. For wind detection, coherent detection can obtain accurate spectral information in the troposphere [43].

Benefiting from the high SNR of the DIAL channel and accurate wind information of the CDWL channel, the hybrid lidar is built for CO<sub>2</sub> flux estimation.

### 2.3. Principle

By detecting the frequency shift of the Doppler signal in the echo, the measurement of the spatial wind field information can be realized by CDWL [44].

The total differential optical depth (*DOD*) for a single optical path of DIAL lidar is estimated as [30]

$$DOD(R_j) = -\frac{1}{2} \ln \left[ \frac{N(\nu_{on}, R_j)}{N(\nu_{off}, R_j)} \right] = \int_0^{R_j} [\alpha_g(\nu_{on}, R_j) - \alpha_g(\nu_{off}, R_j)] dr, \quad (1)$$

and the *DOD* within a range cell ( $\Delta DOD$ ) from  $R_j$  to  $R_{j+1}$  is expressed as

$$\Delta DOD = DOD(R_{j+1}) - DOD(R_j), \quad (2)$$

where  $\alpha_g$  is the absorption coefficient of the gas under investigation;  $N(\nu_{on}, R_j)$  and  $N(\nu_{off}, R_j)$  are the photon numbers received with the optical frequency of  $\nu_{on}$  and  $\nu_{off}$  with a range of  $R_j$ ;  $\Delta\sigma = \sigma_{on} - \sigma_{off}$  is the differential absorption cross-section, taken from HITRAN2020 [45],  $\Delta R = R_{j+1} - R_j$ ; and  $N$  is number density of the gas under investigation. Therefore, we can derive the gas concentration (in ppm) as

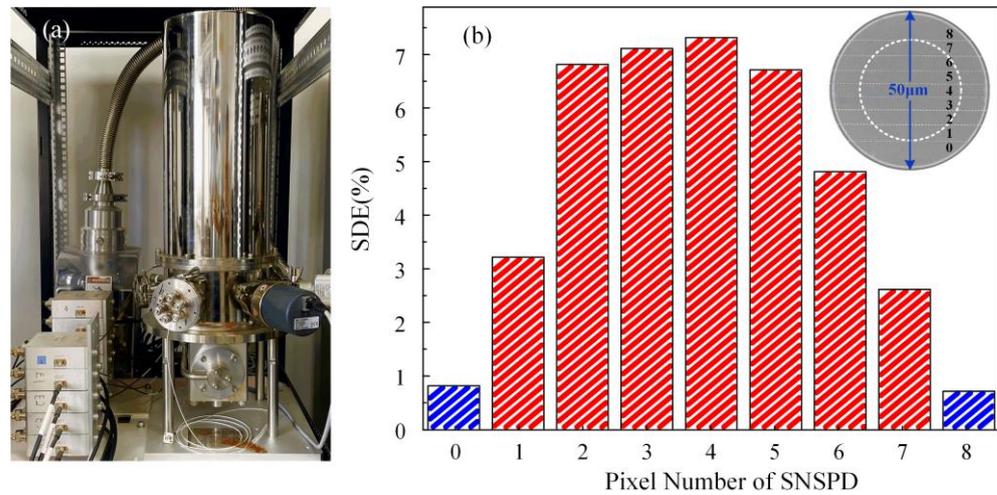
$$\rho = \frac{\Delta DOD \cdot 10^6}{\Delta\sigma \Delta R \cdot N_{air}}, \quad (3)$$

where  $N_{air}$  is the (moist) air number density computed with knowledge of specific humidity, atmospheric pressure, and temperature acquired by a portable, in situ sensor close to the instrument.

### 3. Optimization and Calibration of Optical Receiver

Figure 2a shows the MMF-coupled SNSPD in the DIAL receiver. The active area of the detector is divided into nine pixels [41]. The system detection efficiency (SDE) of SNSPD versus the pixel number is shown in Figure 2b. In the right corner of Figure 2b, a scanning electron microscope (SEM) image of the nine-pixel SNSPD array with large active area (50  $\mu\text{m}$  diameter) is shown. The overall SDE is the sum of the detection efficiency of the nine pixels. The research discovered that the MMF-coupled SNSPD will have the problem of the uneven distribution of photon numbers in the nine pixels, resulting in fluctuations in the detection efficiency and saturation of some pixels [46]. Due to the low count rate, pixel 0 and pixel 8 are only used for boundary detection in the system initialization. As shown in the insert in Figure 2b, the dashed circle indicates the light spot focused on the SNSPD array.

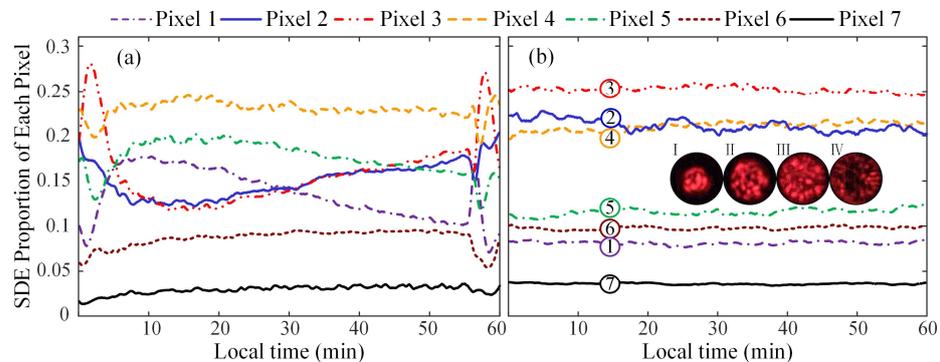
The fluctuation of the SDE is found once disturbance is added to the connecting MMF between the telescope and the SNSPD. Meanwhile, it was found that the SDE of SNSPD is affected by ambient temperature change. For the DIAL technique, as shown in Equation (5), the accuracy of derived gas concentration relies heavily on the stability of the detector. Thus, it is necessary to stabilize and calibrate the optical detector.



**Figure 2.** (a) System photo of SNSPD; (b) SDE as a function of the pixel number. SEM image of nine-pixel SNSPD array with 50  $\mu\text{m}$  circular active area is shown in the right corner.

### 3.1. Mode Scrambling of Multimode Fiber

The perturbation of the MMF will cause light scattering and the redistribution of the power among the guided modes inside the MMF, resulting in different spot distribution in the SDE. Figure 3a shows the SDE proportion of each pixel of the SNSPD (normalized by the total SDE). Due to the low count rate, pixel 0 and pixel 8 are not shown in the figure. It can be seen that the SDE of pixels 1–7 fluctuates with time, especially when the fiber is touched at about the 3rd and 58th minutes.



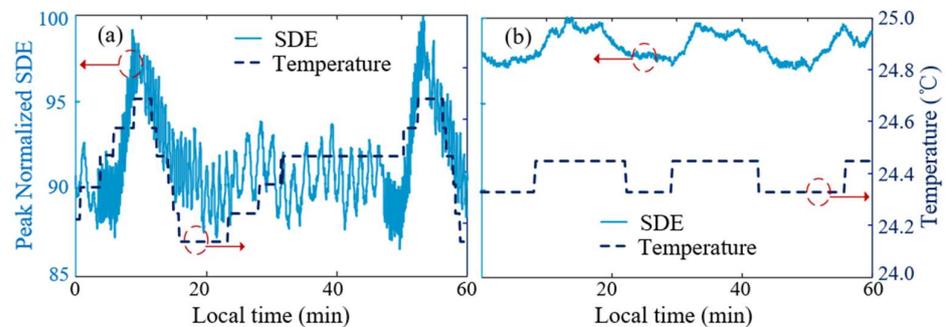
**Figure 3.** (a) SDE proportion of each pixel without mode scrambling. (b) SDE proportion of each pixel with mode scrambling. Images (I–IV) are four spot photos taken after adjusting the mode scrambler to different degrees.

To reduce the impact of vibration on SDE, a mode scrambler (Newport, FM-1) is mounted on the connecting fiber between the telescope and the SNSPD. It presses the fiber between specially designed corrugated surfaces to cause the microbending of the fiber, which dramatically increases mode coupling among guided modes (mode scrambling) and the coupling of high-order guided modes to radiation modes (mode filtering). Stable modal distribution in the MMF is then achieved. Meanwhile, negligible insertion losses are introduced. By observing the light spots emitted from the MMF, the mode scrambler is adjusted to the optimum degree. Figure 3b shows the SDE with optimal microbending. In the middle of Figure 3b, the images (I–IV) are four spot photos taken after adjusting the mode scrambler to different degrees. The laser was captured by a photosensitive card. Image (I) is the light spot without microbending. Image (II) is the light spot with slight microbending. Image (III) is the light spot with optimal microbending. Image (IV) is the light spot with excessive microbending. It can be seen that in Image (III), the area of the light spot is the largest, and the distribution is nearly uniform. After mode scrambling, the

fluctuation between the seven pixels of the SNSPD is significantly suppressed, making the SDE drift tenderly along the time axis.

### 3.2. Temperature Control

Experiments show that the SDE of SNSPD is also affected by ambient temperature. With the core chip working at a temperature of 2.3 K, the performance of SNSPD is not easily affected by ambient temperature. After a series of experiments, it was found that the MMF between the telescope and the SNSPD is affected by temperature. In the experiments, the MMF is exposed to ambient atmosphere. When the temperature in the laboratory changes under the function of the air conditioner (AC), the SDE shows a rapid change and a certain periodicity, as shown in Figure 4a. In Figure 4a,b, red circles and arrows are used to indicate the ordinates corresponding to the two curves. When the temperature changes within the range of 0.7 °C, the peak–valley fluctuation of the SDE reaches about 13%. Here, during the experiment, no mode scrambler was used. Therefore, the wind from the AC causes the vibration of the fiber, resulting in a high-frequency jitter of SDE.



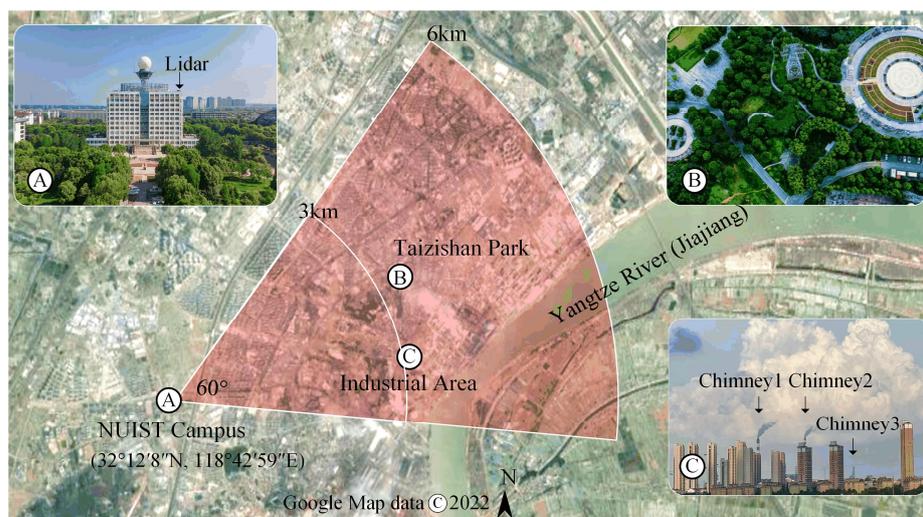
**Figure 4.** (a) Peak-normalized SDE without temperature control; (b) peak-normalized SDE with temperature control. Red circles and arrows are used to indicate the ordinates corresponding to the two curves.

To suppress the effect of temperature on SDE, temperature control for the MMF is performed. The MMF is inserted into a soft water pipe, in which the water temperature is controlled. Thus, the vibration of the MMF is isolated, and the temperature of the MMF is controlled. As shown in Figure 4b, the fluctuation of the SDE curve changes from a fast jitter to a tender drift, which can be compensated for in the DIAL data processing. When the temperature changes within  $\pm 0.1$  °C, the SDE change is controlled with  $\pm 1.5\%$  over 1 h.

## 4. Experiments and Results

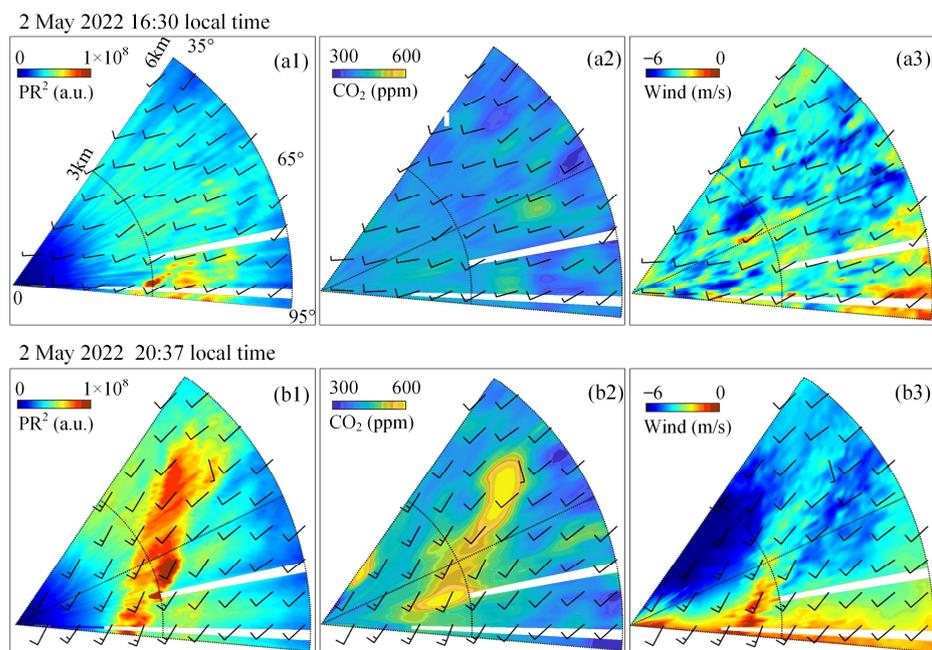
### 4.1. Horizontal CO<sub>2</sub> Distribution and Wind Field

The field experiment is performed in Nanjing City, Jiangsu province, China (32°12'8"N 118°42'59"E). The observation period is from 2 May to 3 May 2022. Horizontal plan position indicator (PPI) scanning is performed to obtain spatial distribution and transport of CO<sub>2</sub>. As shown in Figure 5, the lasers are emitted horizontally at Nanjing University of Information Science and Technology (NUIST) at an altitude of 30 m. With a detection range of 6 km, the scanning angle spans from 35° to 95° by a step of 1°. The accumulation time along one radial direction is 15 s. Three typical areas are covered by the lidar scan (i.e., the NUIST campus, Taizishan Park, and an industrial area). If not specified, local time is used.



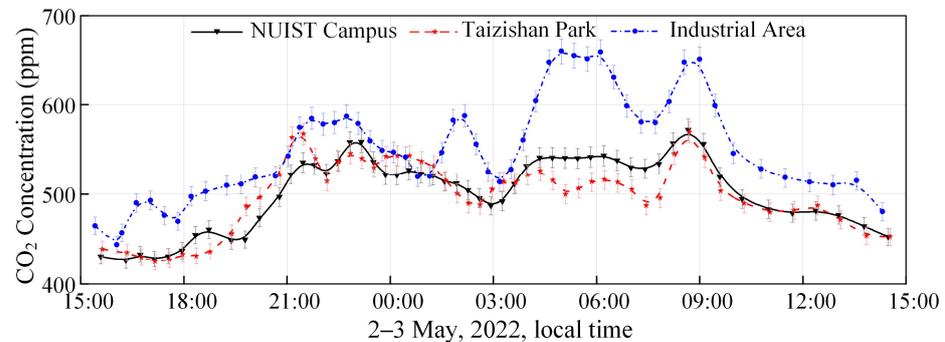
**Figure 5.** Illustration of measurement areas. (A) indicates the NUIST campus, (B) is Taizishan Park, and (C) represents an industrial area.

Figure 6 is horizontal scanning results at two moments. Figure 6a1–a3 show the range-corrected backscatter signal  $PR^2$ ,  $CO_2$  concentration, and radial wind vector at 16:30. Figure 6b1–b3 show corresponding results at 20:37.  $PR^2$  is the product of the power of the backscatter signal and the square of the range. The sign of wind is defined as positive when the movement is toward the lidar, and vice versa [42]. The backscatter in Figure 6a1 is relatively uniform. Figure 6a2 shows low  $CO_2$  concentration during light pollution conditions. The wind-driven plumes of intensified backscatter  $PR^2$  and  $CO_2$  concentration in Figure 6b1,b2 are consistent with the wind field. Considering that there is an industrial area in the scanning area, the local high concentration is most likely the emissions from the factories.



**Figure 6.** Horizontal scanning results on 2 May 2022 in Nanjing. (a1–a3) are backscatter signal  $PR^2$ ,  $CO_2$  concentration, and radial velocity at 16:30. (b1–b3) are at 20:37. The blank areas in the fan charts are caused by hitting hard targets (Chimney 1 and Chimney 2 in Figure 5). The wind barbs represent the wind speed and direction.

To further analyze the diurnal variation in the CO<sub>2</sub> concentration, the results of diurnal CO<sub>2</sub> concentrations in three areas are shown in Figure 7. For the three areas, CO<sub>2</sub> concentrations begin to increase at 18:00 and remain at high values during the night. Then, the concentrations gradually decrease after 09:00 in the morning. Thanks to the high greenery-coverage rates at the NUIST Campus and in Taizishan Park, the CO<sub>2</sub> concentration is lower than that in the industrial area.



**Figure 7.** The diurnal variation in CO<sub>2</sub> concentrations at three typical locations. Error bars indicate the 1 $\sigma$  standard deviation.

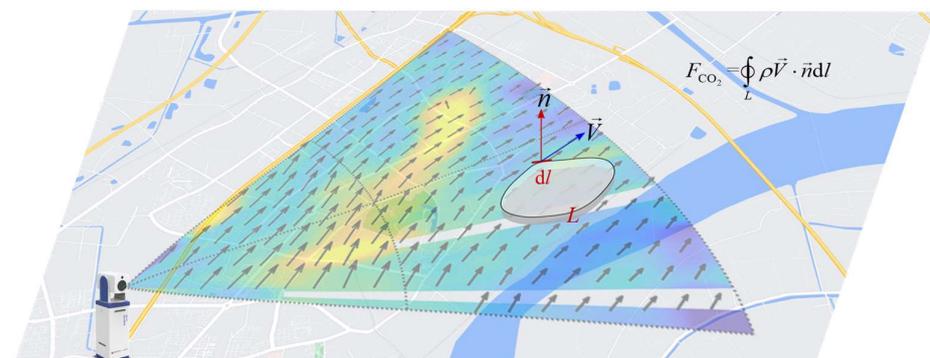
#### 4.2. Horizontal Net Flux

To assess the transport and emission of CO<sub>2</sub> in different regions, an estimation of CO<sub>2</sub> horizontal net flux is required. Using the horizontal slice of the CO<sub>2</sub> concentration distribution at a certain height, a method is proposed to calculate the local horizontal net CO<sub>2</sub> flux by integrating the CO<sub>2</sub> transport vector over a closed boundary of the area of interest.

Figure 8 is the illustration of the horizontal net flux calculation, defined as

$$F_{CO_2} = \oint_L \rho \vec{V} \cdot \vec{n} dl, \quad (4)$$

where  $\vec{V}$  is the wind velocity vector,  $\vec{n}$  is the normal vector of the boundary,  $\rho$  is the CO<sub>2</sub> concentration, and  $l$  is the length of the boundary of the area under investigation. Horizontal net flux  $F_{CO_2}$  represents the regional CO<sub>2</sub> horizontal transport at a certain height. A positive value means CO<sub>2</sub> output is higher than the input.



**Figure 8.** Schematic diagram of horizontal net flux. The black arrow represents the wind vector.

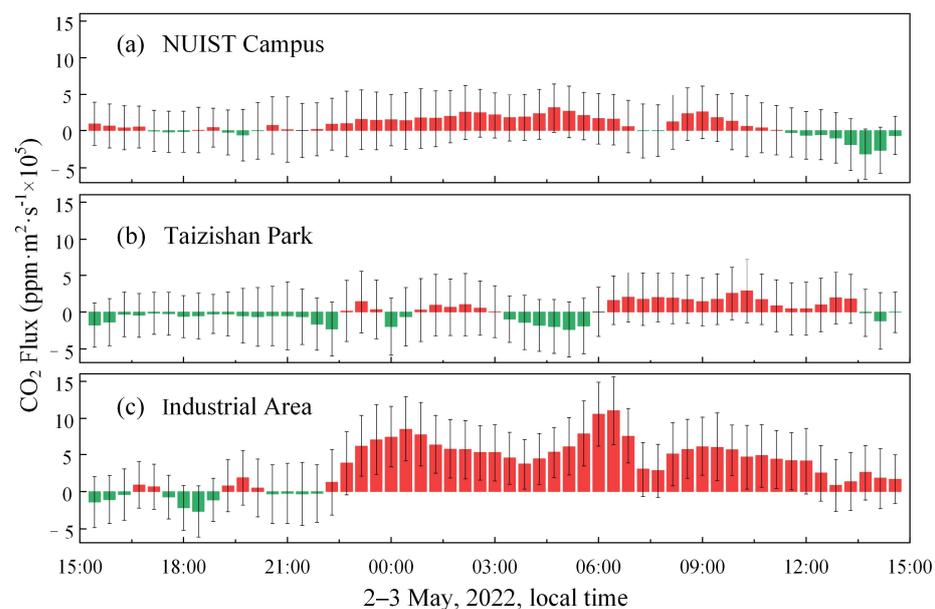
According to Equation (4), the boundaries of the three areas aforementioned are chosen. The area is roughly defined in polar coordinates in the following format:  $A \in [(r_1, r_2), (\theta_1, \theta_2)]$ , where  $A$  is the area under investigation,  $r_1$  and  $r_2$  are the start and end radii, and  $\theta_1$  and

$\theta_2$  define the angle span. In this experiment, the areas of the campus, park, and industrial area are given as:

$$\begin{aligned} A_C &\in [(0.6 \text{ km}, 1.6 \text{ km}), (50^\circ, 60^\circ)], \\ A_P &\in [(3.0 \text{ km}, 4.0 \text{ km}), (59^\circ, 64^\circ)], \\ A_I &\in [(3.0 \text{ km}, 4.0 \text{ km}), (84^\circ, 90^\circ)]. \end{aligned}$$

As shown in the satellite photo of Figure 5, many white plumes can be seen in the lower part of the scanning area. Chimney 1 and Chimney 2 in Figure 5 are located at 2–3 km. Since the two chimneys are conspicuous, the emission is critically monitored and controlled. In this work, we are interested in the unknown emission sources. As shown in Figure 6a1, there are some emission sources in 3–4 km. Thus,  $A_I$  is selected as the industrial area to estimate flux.

The diurnal measurements of horizontal net fluxes in three typical areas are shown in Figure 9. The red bars represent positive flux, the green bars represent negative flux. Clearly,  $\text{CO}_2$  horizontal transport modes vary widely in different local areas. The results indicate different characteristics of horizontal net  $\text{CO}_2$  fluxes in the different local areas. For most of the time during the experiment,  $\text{CO}_2$  flux is positive in the industrial area. On the contrary, on the campus and in the park,  $\text{CO}_2$  fluxes fluctuate around zero, indicating that  $\text{CO}_2$  output is close to the input in these areas. The horizontal net fluxes averaged over 24 h of the campus, the park, and the industrial area are  $0.7 \times 10^5 \text{ ppm}\cdot\text{m}^2\cdot\text{s}^{-1}$ ,  $0.1 \times 10^5 \text{ ppm}\cdot\text{m}^2\cdot\text{s}^{-1}$ , and  $3.5 \times 10^5 \text{ ppm}\cdot\text{m}^2\cdot\text{s}^{-1}$ , respectively. From the estimated  $\text{CO}_2$  horizontal net fluxes, the carbon sinks and sources can be identified.



**Figure 9.** The diurnal variation in horizontal net flux in three typical areas: (a) NUIST campus, (b) Taizishan Park, and (c) industrial area. Error bars indicate the  $1\sigma$  standard deviation. The red bars represent positive flux, the green bars represent negative flux.

To estimate the precision of flux, the standard deviation is calculated. The integration of Equation (4) can be expressed as the form of discrete summation as

$$\sum_i \rho_i V_i \Delta t_i = \sum_i F_{\text{CO}_2, i}, \quad (5)$$

where  $V_i$  is the projected wind speed along the normal direction of the area boundary. Therefore, the measurement variance of the horizontal net flux can be calculated with

$$\sigma_{F_{CO_2}}^2 = \sum_i F_{CO_2,i} \left( \frac{\sigma_{\rho_i}^2}{\rho_i^2} + \frac{\sigma_{V_i}^2}{V_i^2} \right), \quad (6)$$

where  $\sigma_{\rho_i}$  and  $\sigma_{V_i}$  are the standard deviation of the CO<sub>2</sub> concentration and the projected wind speed, respectively.  $\sigma_{\rho_i}$  at 2 km is about 2.1% [30],  $\sigma_{V_i} < 0.6$  m/s within a measure distance of 6 km [42], and detailed information is shown in our previous works. The total standard deviation of CO<sub>2</sub> flux  $\sigma_{F_{CO_2}}$  based on Equation (6) is jointly determined by the  $\sigma_{\rho_i}$  and  $\sigma_{V_i}$  and the length of the boundary to be measured. The total standard deviation of CO<sub>2</sub> flux  $\sigma_{F_{CO_2}}$  is then calculated based on Equation (6) and shown as error bars in Figure 9.

The horizontal net flux can help to trace the source of CO<sub>2</sub>. It shows whether the CO<sub>2</sub> on the horizontal plane is a net input or a net output along the horizontal wind vector at a certain height above the interested area. The measured flux data show that the horizontal net flux in the industrial area is indeed much higher than that in the campus and the park, proving the feasibility of our method. To obtain the precise emission in the three-dimensional (3D) space quantitatively, it is necessary to perform 3D scanning measurements.

## 5. Conclusions

A lidar system incorporating DIAL and CDWL was developed. The two receivers share a transmitter so that the same atmospheric volume is probed for both velocity and concentration measurements. Due to the high signal-to-noise ratio of the SNSPD, the DIAL channel shows high sensitivity in CO<sub>2</sub> detection. The CDWL provides wind field information which is helpful for the traceability of CO<sub>2</sub> emission and the forecast of its transportation. Through the optimization and calibration of the DIAL receiver, the stability of the SDE of SNSPD is significantly improved. Angular scanning in a horizontal plane gives access to CO<sub>2</sub> concentration and horizontal wind velocity mapping over a large area (6 km range and 60° angular coverage). The CO<sub>2</sub> concentration and wind velocity are then used to estimate CO<sub>2</sub> horizontal net fluxes in characteristic locations including an industrial area. The results show correlations among the different signals. The CO<sub>2</sub> daily cycle is observed, and a local CO<sub>2</sub> plume emitted by the industrial plant is captured by the lidar.

In conclusion, the developed lidar system incorporating DIAL and CDWL proved effective in monitoring real-time CO<sub>2</sub> concentration and estimating the horizontal net fluxes for local CO<sub>2</sub> emission and transport events. The horizontal net flux can certainly help to trace the source of CO<sub>2</sub>, while the 3D spatial distributions of CO<sub>2</sub> concentration and wind vector are necessary to obtain precise emission measurements in the 3D space quantitatively. By scanning the slices of a CO<sub>2</sub> plume from a source located downwind of the lidar and incorporating orthogonal wind, 3D CO<sub>2</sub> flux can be calculated and verified [38,39]. It is recommended that the boundary of the area of interest be selected according to the actual shape of the area for fine calculation. Next, comparison experiments of the CO<sub>2</sub> 3D flux are planned. The horizontal net flux can help trace the source of CO<sub>2</sub>. However, the horizontal net flux defined in the present work is only the CO<sub>2</sub> horizontal transport at a certain height. In the near future, 3D CO<sub>2</sub> flux estimation can be realized with multi-layer scanning experiments.

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